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UV camera conceptual designs for TMT Fiber WFOS

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ABSTRACT

This paper discusses refractive, reflective and catadioptric designs for the Thirty Meter Telescope Fiber Wide Field Optical Spectrograph (WFOS) instrument concept. Custom macros were written to evaluate performance at the detector plane with the grating at the pupil as a function of fiber position in the pseudo-slit and wavelength, and a tolerance analysis has been performed for each design based on best engineering practices to assess performance robustness against opto-mechanical errors. The catadioptric camera appears to provide the best compromise in this regard.

Keywords: Wide Field Optical Spectrograph (WFOS) instrument, fiber spectrograph, camera design

1. INTRODUCTION

WFOS [1] is a Wide Field Optical Spectrograph, planned to be one of the two first-light instruments for the Thirty Meter Telescope (TMT), together with IRIS, an Infrared Imaging Spectrograph. WFOS is in its conceptual design phase since August 2017. Fiber and slicer concepts are investigated by the WFOS team, and a down-select review is planned towards the end of 2018. This paper describes 4 designs for the ultraviolet (UV) camera of the fiber concept based on first-order spectrograph parameters at the beginning of the conceptual design phase. Two refractive designs are discussed, which are an evolution of previous designs developed by Nick Konidaris and Rebecca Bernstein, a 5-mirror anastigmat (5MA) is discussed, which is an evolution of a freeform design developed by Dave Shafer, and a 3-element catadioptric design is discussed, which is an evolution of a design developed by Bernard Delabre for the MOONS camera. Designs were optimized individually as subsystem components of the whole modular spectrograph instrument. Custom macros were written to evaluate performance at the detector plane for each design with the grating at the pupil as a function of fiber position in the pseudo-slit and wavelength. A tolerance analysis has been performed for each design based on best engineering practices. Iteration with mechanical engineering is required for further refinement of tolerances.

The fiber WFOS straw-man design is inspired from the DESI spectrograph [2][3], which is a 5,000 fiber spectrograph at the Kitt Peak National Observatory (KPNO) and from the MOONS spectrograph [4], which is a 1,000 fiber spectrograph at the Very Large Telescope (VLT). In the fiber WFOS spectrograph concept, the TMT Exit Pupil (XP) would be coupled onto thousands of fibers via microlens arrays (MLAs) positioned via a robotic positioner covering an 8arcmin diameter field of view (FoV) on the TMT Nasmyth focal surface. Light from the TMT XP coupled into fibers at the Nasmyth focal surface would be transported to several (up to nine) rack-mounted replicated modular spectrographs. Each spectrograph would have 3 or 4 arms (see Figure 1), each arm optimized for a specific wavelength band, and the spectrograph would have a total wavelength coverage ranging from $\lambda_{\min} = 0.31\mu\text{m}$ to $\lambda_{\max} = 1.0\mu\text{m}$ and would provide a spectral resolution $R(\lambda) = \lambda / \Delta\lambda = 5,000$ across the instrument wavelength band. At the input of each modular spectrograph would be a curved pseudo-slit (object surface) containing hundreds of fibers (circular extended objects) stacked next to each other. The pseudo-slit surface vertex would be at the front focal point of an on-axis spherical collimating mirror whose center of curvature (CC) would coincide with that of the pseudo-slit (both surfaces would be concentric). At the common CC would be a Pupil Plane (PP) located a distance $2f_{\text{col}}$ from the collimator, where $2f_{\text{col}}$ denotes the collimator focal length. Because the aperture stop is at the CC of the spherical collimator, the

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spherical mirror does not generate coma or astigmatism but only spherical aberration, which can be compensated by the camera since spherical aberration is field independent. An illustration is provided in Figure 1 (the pseudo-slit is in the x-direction and the camera is modeled as a paraxial lens). All chief rays leave the pseudo-slit (propagating virtually from the common CC) at normal incidence, intercept the collimator at normal incidence, and are retro-reflected along the same ray path onto the pseudo-slit. In this on-axis design, the pseudo-slit thus obscures a few percent of the reflected collimated beam. The collimator re-images the PP to a distance $2f_{\text{col}}$ from the mirror (2f imaging), where a tilted grating is placed to disperse light from each fiber in the pseudo-slit into a spectrum (Y direction on the detector).

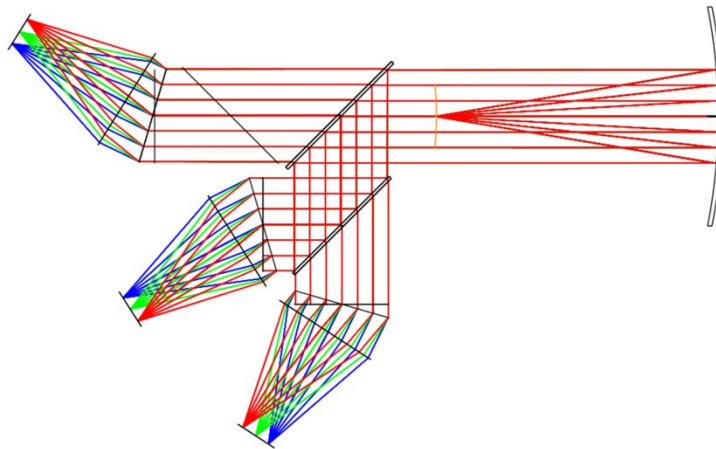


Figure 1: Layout of a modular 3-channel fiber spectrograph.

In this paper, we are concerned with the most challenging ultraviolet (UV) arm of such modular spectrograph, with waveband

$$\lambda_1 = 0.31\mu\text{m}, \quad \lambda_2 = 0.45\mu\text{m}, \quad \lambda_0 = 0.38\mu\text{m} \quad (1.1)$$

where λ_0 denotes the primary wavelength at which focal lengths are specified. For maximum grating efficiency versus wavelength (minimum angular deviation), the spectrograph is designed in Littrow configuration [5][6]. In this configuration, the diffraction angle of the chief ray of the first diffraction order at the primary wavelength $\beta(\lambda_0) > 0$, is equal to the tilt angle of the grating, $\alpha > 0$, as illustrated in Figure 2. The angle between the collimator axis and the camera axis is $\psi = \alpha + \beta(\lambda_0)$. In this paper, a grating period equal to $\nu = 1.475\text{ln} / \mu\text{m}$ is assumed. The diffraction angle, $\beta(\lambda)$, is related to the grating tilt angle by the grating equation:

$$\beta(\lambda) = \sin^{-1} [m_d \nu \lambda - \sin(\alpha)], \quad (1.2)$$

where m_d denotes the diffraction order and ν the grating period. To first-order, the chief ray diffraction angle $\beta(\lambda)$ in (1.2) may be linearized with respect to the grating tilt angle α and wavelength λ :

$$\beta(\lambda)[\text{deg}] \sim \frac{m_d \nu \lambda}{\pi} 180[\text{deg}] - \alpha[\text{deg}] \quad (1.3)$$

The Littrow configuration is found by setting $\beta(\lambda_0) = \alpha$ in (1.2) and solving for α :

$$\begin{aligned} \beta(\lambda_0) - \alpha &= 0 \Rightarrow \alpha = \beta(\lambda_0) = \sin^{-1} [m_d \nu \lambda_0 - \sin(\alpha)] \\ \Rightarrow \sin(\alpha) &= m_d \nu \lambda_0 - \sin(\alpha) \Rightarrow \sin(\alpha) = \frac{m_d \nu \lambda_0}{2} \\ \Rightarrow \alpha &= \sin^{-1} \left[\frac{m_d \nu \lambda_0}{2} \right] = 16.275126^\circ \end{aligned} \quad (1.4)$$

Plots of chief ray diffraction angle versus wavelength $\beta(\lambda)$ and of its change versus wavelength $d\beta/d\lambda$ are provided in Figure 3. The camera field of view (FoV) along the dispersion direction (Y-direction) is given by

$$\text{FoV}_y = \beta(\lambda_2) - \beta(\lambda_1) = 12.4^\circ \quad (1.5)$$

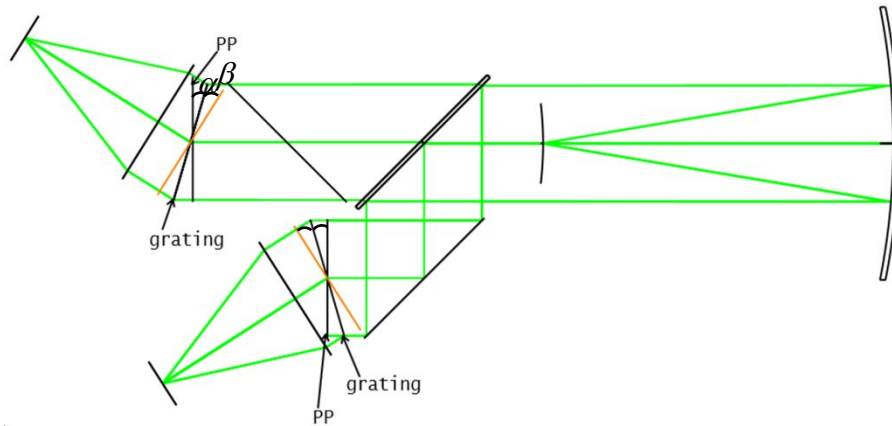


Figure 2: Littrow spectrograph configuration for maximum diffraction grating efficiency.

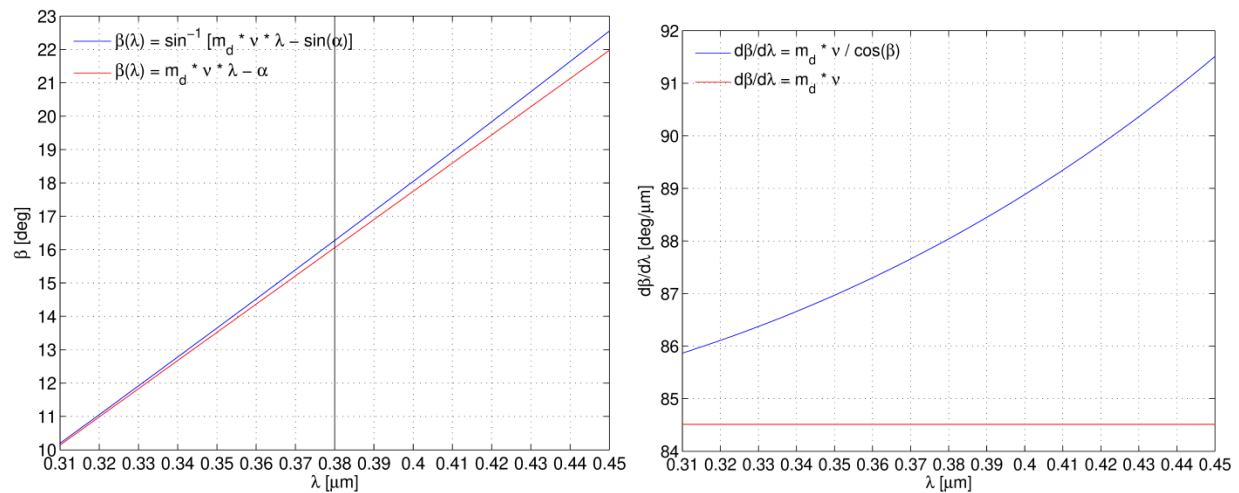


Figure 3: Left: chief ray diffraction angle versus wavelength. Right: change in chief ray diffraction angle with wavelength.

A driving first-order property is the spectrograph paraxial transverse magnification m whose value was chosen based on the DESI spectrograph design. Namely, the spectrograph would image a $100\mu\text{m}$ diameter fiber object onto a first-order circular image of diameter $45\mu\text{m}$ (i.e. three $15\mu\text{m}$ pixels), i.e.

$$m(\lambda_0) = \frac{h'(\lambda_0)}{h} = -\frac{f_{\text{cam}}(\lambda_0)}{f_{\text{col}}} = -0.45 \quad (1.6)$$

where $h = 50\mu\text{m}$ denotes object height, $h' = -22.5\mu\text{m}$ image height, and f_{cam} is the camera focal. The first-order image diameter $2|h'|$ is an important first-order parameter; it places a limit on spectral resolution: resolving two wavelengths separated by a spectral resolution element $\Delta\lambda$ requires the two images to be separated along the dispersion direction by a spatial resolution element Δx at least as large as their diameter:

$$\Delta x(\lambda_0) \geq 2|h'(\lambda_0)| \quad (1.7)$$

The ultraviolet band places serious constraints on the available glasses for the camera. It appears that only Calcium Fluoride (CaF₂) and Fused Silica (SiO₂) glasses have a transmittance greater than 99.8% at these wavelengths for 10mm thick samples, see for instance [21]. In this paper, we are considering a 6K x 6K sensor with 15 μ m pixels, providing a square $L' \times L'$ image size with $L' = 90$ mm, e.g. a 3x3 mosaic of the e2v CCD230-42 [21]. Given the value for the spectrograph transverse magnification, one finds that a $L = L' / |m(\lambda_0)| = 90 / 0.45 = 200$ mm pseudo-slit fits the image size.

2. BLUE CHANNEL CAMERA REQUIREMENTS

2.1 First-order properties

Driving design parameters for the blue camera flow down from the following top-level spectrograph parameters:

1. The camera focal length f_{cam} is defined such that its product with the tangent of the angular resolution element $\Delta\beta$ (angle between 2 resolvable wavelengths) is equal to the spatial resolution element Δx along the dispersion direction as given by (1.7) (linear distance on the detector between 2 resolvable wavelengths, i.e. spectral FWHM):

$$f_{\text{cam}}(\lambda_0) \tan(\Delta\beta(\lambda_0)) = \Delta x(\lambda_0) \quad (1.8)$$

The angular resolution element $\Delta\beta$ is obtained by differentiating the grating equation (1.2) with respect to wavelength, which yields:

$$\Delta\beta(\lambda_0) = \frac{m_d v \lambda_0}{R(\lambda_0) \cdot \cos(\beta(\lambda_0))} \quad (1.9)$$

In the limit of small $\Delta\beta$, we have $\tan(\Delta\beta) \sim \Delta\beta$, and (1.8) can be rewritten:

$$f_{\text{cam}}(\lambda_0) = \Delta x(\lambda_0) \cdot R(\lambda_0) \cdot \frac{\cos(\beta(\lambda_0))}{m_d v \lambda_0} \quad (1.10)$$

For the Littrow configuration, (1.10) simplifies to:

$$f_{\text{cam}}(\lambda_0) = \Delta x(\lambda_0) \cdot R(\lambda_0) \cdot \frac{1}{2 \tan(\alpha)} = 392 \text{mm} \quad (1.11)$$

The fiber WFOS instrument is required to have a spectral resolution equal to $R(\lambda_0) = \lambda_0 / \Delta\lambda = 5,000$ (i.e. 0.076nm wavelength resolution around 380nm), which for the choice of grating angle and spectrograph magnification leads to a 392mm camera focal length at the primary wavelength and $\Delta\beta(\lambda_0) \sim 24$ arcsec.

2. From (1.6), the collimator focal length must be longer than the camera focal length by a factor $1/|m(\lambda_0)|$, leading to a collimator focal length of 872mm:

$$f_{\text{col}} = \frac{f_{\text{cam}}(\lambda_0)}{|m(\lambda_0)|} = 872 \text{mm} \quad (1.12)$$

3. The collimator should be faster than the MLA to account for focal ratio degradation (FRD) introduced by the fiber [9]. Based on the DESI design, a microlens (ML) focal ratio equal to 3.2 is adopted, and a collimator focal ratio of 3.0:

$$f_{\# \text{ML}}(\lambda_0) = 3.2, \quad f_{\# \text{col}} = 3.0 \quad (1.13)$$

As a side note, the ML focal length can be calculated from the imaging equation since the object (TMT XP) distance from the TMT FP and the ML magnification are known. The TMT XP is located at a distance $z_{\text{xp}} = -46,386.61$ mm from the TMT FP and its semi-diameter is equal to $h_{\text{xp}} = 1,546.2$ mm. The required ML magnification to image a point

on the TMT XP perimeter onto a first-order image of height equal to $h'_{XP} = -0.05\text{mm}$ is thus $m_{ML} = h'_{XP} / h_{XP} = -0.1 / 3,092.4 = -(3.2337) \cdot 10^{-5}$. Since image and object locations are related by magnification $m_{ML} = (z'_{XP} / n') / (z_{XP} / n)$, we have $z'_{XP} = 1.5\text{mm}$, and therefore the ML optical power is given by $\phi_{ML} = 1 / f_{ML} = \Delta \{n / z_{XP}\} = n' / z'_{XP} - n / z_{XP} = 0.6668 / \text{mm}$, leading to $f_{ML} = 1.5\text{mm}$. Given the focal ratio value given in eq.(1.13), the ML diameter is equal to $d_{ML} = f_{ML} / f_{\#ML} = 0.4688\text{mm}$, which corresponds to an angular subtense equal to $\theta_{ML} = d_{ML} / f_{ML} = 0.215\text{arcsec}$. Combining (1.12) and (1.13) yields the camera Entrance Pupil (EP) size:

$$D_{EP} = f_{col} / f_{\#col} = 291\text{mm} \quad (1.14)$$

Combining (1.12) and (1.13) yields the camera focal ratio:

$$f_{\#cam}(\lambda_0) = f_{cam}(\lambda_0) / D_{EP} = 1.35 \quad (1.15)$$

The camera field of view along the spatial (pseudo-slit angular subtense) direction can be calculated as follows. For the spatial direction, for a flat object surface, we have $f_{col} \tan(\text{FoV}_x / 2) = L / 2 = 100\text{mm}$, hence $\text{FoV}_x / 2 = 6.54^\circ$. Taking into account the curvature of the object surface, a value equal to $\text{FoV}_x / 2 = 6.59^\circ$ is obtained, hence the field of view along the spatial direction is given by:

$$\text{FoV}_x = 13.2^\circ \quad (1.16)$$

The spatial spread in the dispersion direction for the on-axis fiber is given by:

$$l_y = 2f_{cam}(\lambda_0) \tan(\text{FoV}_y / 2) = 84.93\text{mm} \quad (1.17)$$

where FoV_y is given in (1.5). A real ray-trace from the curved object surface returns a diagonal field of view equal to:

$$\text{FoV} = 18.6^\circ \quad (1.18)$$

It is clear that the camera speed, large FoV and wavelength range pose significant design challenges.

2.2 Performance requirements

The spectrograph performance metric is encircled energy (EE). The requirement is not well defined at this stage of the CODP, but an end-to-end value for the spectrograph of 90% EE inside the first-order image of a fiber diameter ($h' = -22.5\mu\text{m}, h = 50\mu\text{m}$) over the field and wavelength range would be excellent. This performance requirement is extremely ambitious, and corresponds to near-diffraction limited performance (below half wave RMS wavefront error (WFE)). In angular space, the $h = 50\mu\text{m}$ circular fiber radius subtends an angle θ_{obj} satisfying $f_{col} \tan(\theta_{obj}) = h$. The angular subtense of the fiber diameter (object) is then:

$$2\theta_{obj} = 23.65\text{arcsec} = (6.57) \cdot 10^{-3} \text{deg} \quad (1.19)$$

This value matches $\Delta\beta(\lambda_0)$ and is used as object angular size to compute the Extended Source EE.

2.3 Design constraints

The following constraints are imposed on the design of the camera:

1. The stop should be external at distance of at least 85mm in front of the first element of the camera. This distance is called "pupil relief" (PR).
2. 0% vignetting.
3. The back focal distance (BFD) should be at least 8mm to accommodate the CCD window.

3. REFRACTIVE CAMERA DESIGNS

3.1 Design progression

An 11-element spherical lens (denoted “11Sph-0Asph”) developed by Nick Konidaris [10], and an aspheric lens developed by Rebecca Bernstein using 3 spherical lenses plus 6 aspheric lenses (denoted “3Sph-6Asph”) [11] served as our starting point. The aspheric lenses in Rebecca’s design have the front surface of lens 1, 3, 5, 7, and 8 modeled as the sum of 4th, 6th, and 8th-order radially-symmetric asphericities, i.e.

$$\begin{aligned} \text{sag}(\rho) &= \text{sag}_{\text{conicoid}}(\rho) + a_4\rho^4 + a_6\rho^6 + a_8\rho^8, \\ \rho &= \sqrt{x^2 + y^2}, \quad \text{sag}_{\text{conicoid}}(\rho, K) = \frac{c\rho^2}{1 + \sqrt{1 - (1 + K)c^2\rho^2}} \end{aligned} \quad (1.20)$$

where $c = 1/R$ denotes curvature, R radius of curvature and ρ transverse radial distance. In both design, fused silica (SiO₂) elements are negative elements (negative focal lengths), calcium fluoride (CaF₂) elements are positive elements (positive focal lengths).

- Step1. We started by updating the waveband to the values given in (1.1), scaling both designs to the desired focal length given in (1.11), setting $D_{\text{EP}} = 191\text{mm}$ which yields $f_{\#,\text{cam}} = 2$, and defining a circular field of view of diameter given in (1.18). The grating is not included in the optical model at this stage. All field points within the circular field of view are simulated at all wavelengths, and axial symmetry is assumed. Those two simplifying assumptions will be dropped when analyzing performance of the camera with the grating included at the pupil plane and all fibers in the pseudo-slit simulated. As a starting point, to speed up ray tracing during the optimization procedure, waveband and FoV were sampled at only 3 points (min, max, mid-point). The following constraints were imposed on the design in the merit function (MF):

- thickness of each lens element between 15mm (center or edge) and 120mm (center),
- spacing between elements between 0.5mm (center or edge) and 100mm (center),
- focal length 392mm at the primary wavelength,
- BFD at least 8mm.

Lateral color (LAC, i.e. chromatic change of transverse magnification) was ignored. Pupil integration was performed using Gaussian quadrature (GQ) with 10 rings and 10 arms. This integration method is significantly faster and requires significantly less computer memory than a fine rectangular grid, which typically requires very high sampling to reach percent level fluctuations in MF value as sampling changes. Levenberg-Marquardt damped least squares (DLS) optimization was performed on both designs (convergence is slow and reaching a local minimum takes several hours on an 8-core laptop computer).

- Step2. The entrance pupil diameter (EPD) was increased to $D_{\text{EP}} = 217\text{mm}$ ($f_{\#,\text{cam}} = 1.8$) and both designs were re-optimized, paying close attention to constraints violations.
- Step3. The EPD was increased to $D_{\text{EP}} = 245\text{mm}$ ($f_{\#,\text{cam}} = 1.6$) and both designs were re-optimized.
- Step4. The EPD was increased to $D_{\text{EP}} = 270\text{mm}$ ($f_{\#,\text{cam}} = 1.45$) and both designs were re-optimized.
 - This step required lens center thicknesses of up to 180mm.
- Step5. Both designs were re-optimized for the target EPD i.e. $D_{\text{EP}} = 291\text{mm}$ ($f_{\#,\text{cam}} = 1.35$). The total mass of both designs produced after optimization is 460kg for the 11-element design and 205kg for the 9-element design.
- Step6. The following modifications were made in the MF:
 - The glass minimum center thickness was increased to 25mm and edge thickness to 20mm respectively,
 - The minimum spacing between elements was increased to 1mm.

- A 55deg constraint was imposed on the maximum ray angle of incidence and exitance at each surface to reduce near total internal reflection (TIR) observed at Step5.
- Step7.
 - A maximum total mass constraint of 370kg for 11-element design and of 265kg for the 9-element design was added in the MF.
 - The spacing between elements was allowed to grow up to 200mm.
 - A 10% margin was imposed on the clear semi-diameters of all elements.
 - Pupil relief was allowed to vary between 85-100mm for the 11-element design.
 - The constraint on the maximum ray angle of incidence and exitance was increased to 65deg for the 11-element design.
- Step8.
 - The last element (aspheric field lens) of the 9-element design was removed (the resulting design will be denoted “3Sph-5Asph”).
 - The MF was updated for finer field and wavelength sampling: 11 Y-fields, 11 wavelengths, and both systems were re-optimized.
- Step9.
 - The grating was introduced at the pupil, 11 X-fields and 11 wavelengths were simulated, the MF was updated and both systems were re-optimized.

3.2 Performance Result

3.2.1 Spherical lens with grating and fibers in pseudo-slit

3.2.1.1 Nominal performance

In this Section, an in-depth performance analysis of the lens including the grating and fibers in the pseudo-slit is discussed. The simulated 11 x-field points sampling the spectrograph pseudo-slit have coordinates given by $\theta_x = \{0^\circ, \pm 1.32^\circ, \pm 2.64^\circ, \pm 3.96^\circ, \pm 5.28^\circ, \pm 6.6^\circ\}$. The lens layout and the optical prescription are shown in Figure 4 and Figure 5 respectively. All radii and thicknesses are specified with only 2 significant digits (10 microns accuracy) and the optimization criterion was RMS WFE with respect to centroid over all 11 x-fields and 11 wavelengths, and pupil integration was performed using GQ with 10 rings and 10 arms. Uniform field and wavelength weights were used to build the merit function. As-designed performance results are shown in Figure 6 (performance is symmetric with respect to x-fields since the as-designed lens system is axially symmetric). Sensitivity to BFD and image plane tilt is illustrated in Figure 7. The mean extended source EE drops by 10% for a $\pm 40\mu\text{m}$ BFD error about the nominal value, or for a tilt error equal to $\pm 0.1\text{deg}$.

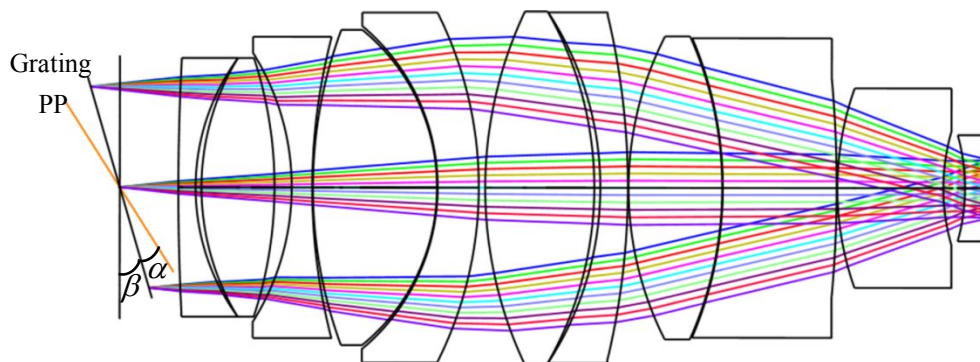


Figure 4: Optical layout and on-axis field Y-fan for the 11Sph-0Asph design including the grating. The global coordinate reference surface is the front surface of the first lens. Rays are colored by wavelength.

	Surf.Type	Comment	Radius	Thickness	Material	Semi-Diameter	Mech Semi-Dia	Conic	Decenter X	Decenter Y	Tilt About X	Tilt About Y
0	OBJECT	Standard	Infinity	Infinity		Infinity	Infinity	0.00000				
1	STOP	Standard	pupil	Infinity		145.50000	145.50000	0.00000				
2	Coordinate Break			0.00000	-	0.00000	-		0.00000	0.00000	16.28000	0.00000
3	Diffraction Grating	grating	Infinity	0.00000		167.385276	-	0.00000	1.475000	-1.000000		
4	Coordinate Break	pupil relief		84.974008	V	0.00000	-		0.000000	0.000000	16.270252	0.000000
5	Standard	lens 1	3580.150000	25.00000	F_SILICA	181.042576	187.106134	0.00000				
6	Standard		316.230000	8.50000		187.106134	187.106134	0.00000				
7	Standard	lens 2	359.140000	105.950000	CAF2	188.742634	194.108742	0.00000				
8	Standard		-598.020000	24.960000		194.108742	194.108742	0.00000				
9	Standard	lens 3	-363.880000	29.750000	F_SILICA	194.494319	217.890790	0.00000				
10	Standard		863.980000	1.00000		217.890790	217.890790	0.00000				
11	Standard	lens 4	656.730000	179.940000	CAF2	223.446955	235.081724	0.00000				
12	Standard		-293.890000	1.00000		235.081724	235.081724	0.00000				
13	Standard	lens 5	-303.680000	59.650000	F_SILICA	233.591268	253.197535	0.00000				
14	Standard		-562.210000	9.290000		253.197535	253.197535	0.00000				
15	Standard	lens 6	595.600000	158.250000	CAF2	260.428708	260.428708	0.00000				
16	Standard		-510.980000	8.680000		255.006529	260.428708	0.00000				
17	Standard	lens 7	-462.250000	39.980000	F_SILICA	253.730901	253.730901	0.00000				
18	Standard		-1069.010000	1.00000		249.354996	253.730901	0.00000				
19	Standard	lens 8	482.820000	135.860000	CAF2	233.906384	233.906384	0.00000				
20	Standard		-535.580000	0.870000		219.204332	233.906384	0.00000				
21	Standard	lens 9	-548.970000	165.110000	F_SILICA	216.636742	216.636742	0.00000				
22	Standard		-1733.130000	0.990000		158.702633	216.636742	0.00000				
23	Standard	lens 10	430.110000	153.730000	F_SILICA	144.283978	144.283978	0.00000				
24	Standard		295.530000	31.380000		82.428781	144.283978	0.00000				
25	Standard	lens 11	-283.410000	24.580000	F_SILICA	76.822599	76.822599	0.00000				
26	Standard		2632.360000	7.840000	V	71.388145	76.822599	0.00000				
27	Coordinate Break			0.000000	-	0.000000	-		0.000000	0.000000	0.000000	0.000000
28	IMAGE	Standard	Infinity	-		63.566902	63.566902	0.00000				

Figure 5: Optical prescription for the 11Sph-0Asph design including the grating.

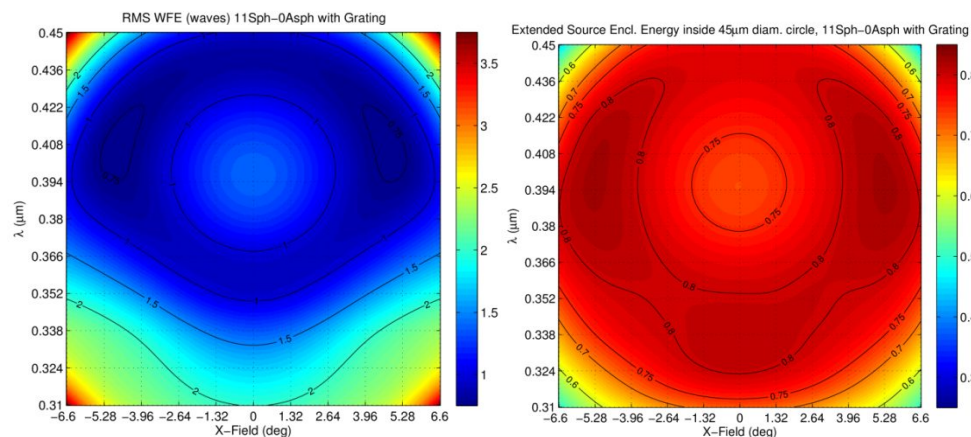


Figure 6: RMS WFE and extended source EE within 45µm diameter versus field and wavelength for the 11-element spherical lens with grating. The RMS WFE map is plotted with color bar on a scale ranging from 0.75 to 3.75 waves, and the EE map from 0.25 to 0.85.

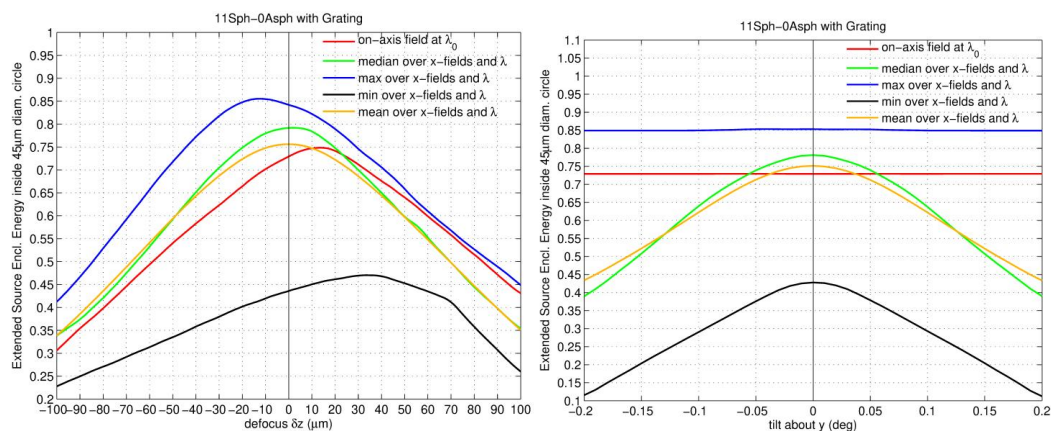


Figure 7: Left: extended source EE within 45µm diameter versus defocus from nominal image plane position. Right: extended source encircled energy sensitivity to detector plane tilt.

3.2.1.2 Tolerance analysis

An in-depth tolerance analysis was performed, considering all x-fields and wavelengths. Each Monte Carlo trial was optimized for RMS WFE over all x-fields and wavelengths. A custom external macro was used to post-process the saved Monte Carlo runs and compute the extended source EE for each field point, wavelength and simulation trial. Since this process is computationally intensive, EE was queried only over an 11x11 grid of points (11 x-fields and 11 wavelengths). The tolerances listed in Table 1 were imposed on the lens based on Optimax manufacturing tolerance chart [12]. Monte Carlo tolerance analysis is critical to understand product cost versus performance [13].

Item	Value	Comment
Radius of curvature	$\pm 0.1\%$ or $\pm 0.05\%$	from sensitivity analysis
Thickness (glass and air)	$\pm 100\mu\text{m}$	
X and Y element decenter	$\pm 50\mu\text{m}$	twice Optimax high-precision thickness tolerance as an estimate for linear distance tolerance, pending mechanical review
Surface irregularity	± 0.2 fringes	Optimax high precision
Surface X and Y tilt, i.e. edge thickness difference (wedge)	$\pm 2.5\mu\text{m}$	Optimax high precision
Element X and Y tilt	$\pm 0.0083\text{deg}$ ($\pm 0.5\text{arcmin}$)	Optimax wedge prism high precision
Index	$\pm 5 \cdot 10^{-4}$	
Abbe number	$\pm 0.8\%$	

Table 1: Opto-mechanical tolerances adopted for the spherical lens tolerance analysis.

Four active compensation strategies were studied in the 1,000 Monte Carlo simulation trials with uniform opto-mechanical error statistics:

- Active BFD adjustment (constrained between 6mm and 13mm)
- Active Pupil Relief adjustment (constrained between 83mm and 90mm)
- Active detector plane X- and Y-tilt adjustment (constrained between -2deg and +5deg)

Figure 8 plots performance versus success rate (defined as the probability over Monte Carlo trials to meet or exceed a given performance level). We find that the median extended source encircled energy over x-fields and wavelengths is slightly worse than on-axis encircled energy at the primary wavelength.

- For a 98% success rate, 35% median extended source encircled energy over x-fields and wavelengths can be expected.
- For a 90% success rate, 43% median extended source encircled energy over x-fields and wavelengths can be expected.
- For a 70% success rate, 51% median extended source encircled energy over x-fields and wavelengths can be expected.

Compensator statistics from the 1,000 Monte Carlo simulations illustrate that the mean pupil relied is very close to 85mm, mean BFD very close to 8mm and mean image tilt about the x-axis close to 6milli-deg (0.36arcmin).

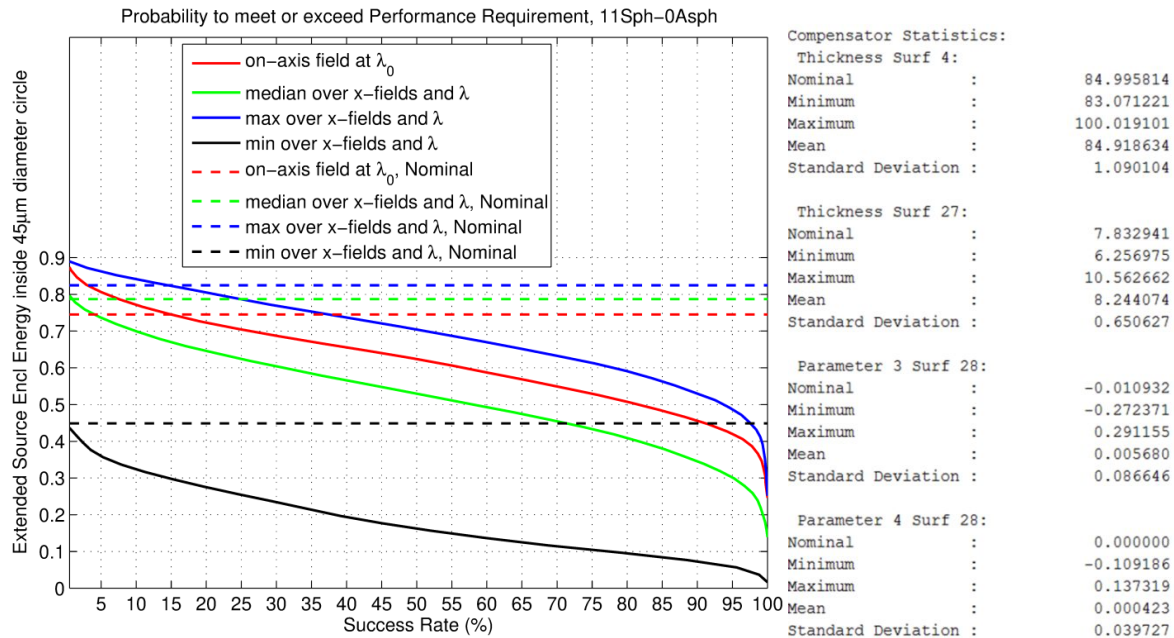


Figure 8: Monte Carlo tolerance results of the spherical lens with grating. 1,000 Monte Carlo trials were performed with uniform opto-mechanical error statistics. Success rate is defined as the probability over simulation trials to meet or exceed a given performance level. Right: compensator statistics for the 11Sph-0Asph design including the grating. The first group is pupil relief, the second is BFD and last two are image plane tilt about the x- and y-axis respectively.

3.2.2 Aspheric lens with grating and fibers in pseudo-slit

3.2.2.1 Nominal performance

In this Section, performance of the aspheric lens with the grating and all fibers in the pseudo-slit is discussed. The lens layout is shown in Figure 9, the optical prescription in Figure 10 and performance results in Figure 11 and Figure 12. The merit function was built with the on-axis and edge x-field points having twice the weight of the other x-fields, and similarly the primary and edge wavelengths having twice the weight of the other wavelengths. Such a weighting provides more uniform performance across fields and wavelengths.

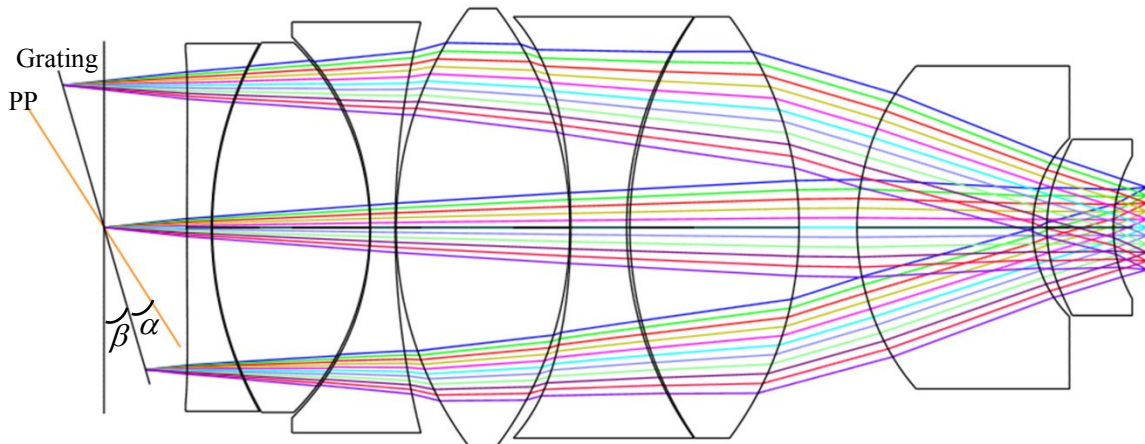


Figure 9: Optical layout and on-axis field Y-fan for the 3Sph-5Asph design including the grating. The global coordinate reference surface is the front surface of the first lens. Rays are colored by wavelength.

	Surf-Type	Comment	Radius	Thickness	Material	Semi-Diameter	Mech Semi-Dia	Conic	Decenter X	Decenter Y	Tilt About X	Tilt About Y
0	OBJECT	Standard ▾	Infinity	Infinity		Infinity	Infinity	0.000000				
1	STOP	Standard ▾	pupil	0.000000		145.500000	145.500000	0.000000				
2	Coordinate Break ▾			0.000000	-	0.000000	-		0.000000	0.000000	16.280000	0.000000
3	Diffraction Grating ▾	grating	Infinity	0.000000		167.385276	-	0.000000	1.475000	-1.000000		
4	Coordinate Break ▾	pupil relief		84.970000 V	-	0.000000	-		0.000000	0.000000	16.270252	0.000000
5	Even Asphere ▾	Lens 1 (Asph)	-7.180000E+04	24.259997	F_SILICA	180.176027	188.422888	0.000000	0.000000	-1.413195E-09	-6.067048E-15	-1.071633E-18
6	Standard ▾		382.860000	1.020000		188.422888	188.422888	0.000000				
7	Standard ▾	Lens 2	374.890000	155.380000	CAF2	189.970163	196.112719	0.000000				
8	Standard ▾		-271.950000	0.640000		196.112719	196.112719	0.000000				
9	Even Asphere ▾	Lens 3 (Asph)	-295.690000	24.970000	F_SILICA	195.824028	212.503384	0.000000	0.000000	-8.903621E-09	5.203451E-14	7.245132E-19
10	Standard ▾		875.860000	1.000000		212.503384	212.503384	0.000000				
11	Standard ▾	Lens 4	375.910000	179.300000	CAF2	227.764641	227.764641	0.000000				
12	Standard ▾		-354.740000	1.000000		227.764641	227.764641	0.000000				
13	Even Asphere ▾	Lens 5 (Asph)	-577.130000	46.870000	F_SILICA	218.451797	218.451797	0.000000	0.000000	-1.043498E-09	-2.161001E-13	4.018886E-19
14	Standard ▾		367.100000	2.980000		218.451797 P	218.451797	0.000000				
15	Standard ▾	Lens 6	375.170000	178.130000	CAF2	218.451797 P	218.451797	0.000000				
16	Standard ▾		-359.990000	59.770000		218.451797 P	218.451797	0.000000				
17	Even Asphere ▾	Lens 7 (Asph)	247.120000	178.340000	F_SILICA	169.495810	169.495810	0.000000	0.000000	-2.987878E-09	8.528943E-14	1.436188E-18
18	Standard ▾		132.920000	14.700000		94.558807	169.495810	0.000000				
19	Even Asphere ▾	Lens 8 (Asph)	160.760000	73.090000	CAF2	93.490148	93.490148	0.000000	0.000000	-2.299681E-08	-3.759925E-13	-3.959274E-16
20	Standard ▾		152.510000	0.000000		74.297175	93.490148	0.000000				
21	Standard ▾		Infinity	41.520000 V		76.878286	76.878286	0.000000				
22	Coordinate Break ▾			0.000000	-	0.000000	-		0.000000	0.000000	0.000000 V	0.000000 V
23	IMAGE	Standard ▾	Infinity	-		64.234636	64.234636	0.000000				

Figure 10: Optical prescription for the 3Sph-5Asph design including the grating.

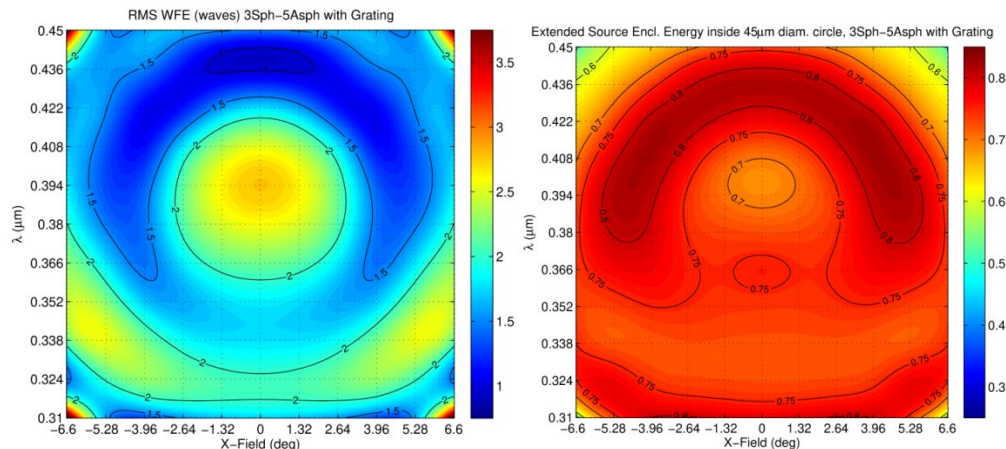


Figure 11: RMS WFE and extended source EE within 45μm diameter versus field and wavelength for the 8-element aspheric lens with grating. The RMS WFE map is plotted with color bar on a scale ranging from 0.75 to 3.75 waves, and the EE map from 0.25 to 0.85.

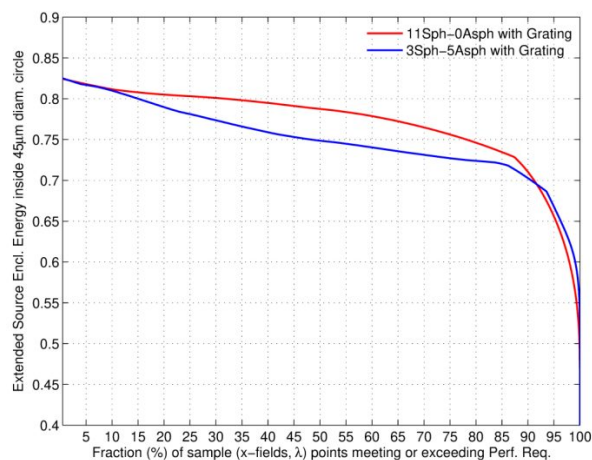


Figure 12: EE inside a 45micron diameter circle at the detector versus fraction of field and wavelength points meeting or exceeding a given performance level for the 11-element spherical lens with grating and the 8-element aspheric lens with grating.

3.2.2.2 Tolerance analysis

Monte Carlo tolerance simulation results are displayed in Figure 13 for the same tolerances (see Table 1) and compensators (PR, BFD and image plane tilt) as for the spherical lens, 1000 simulation trials with uniform error statistics.

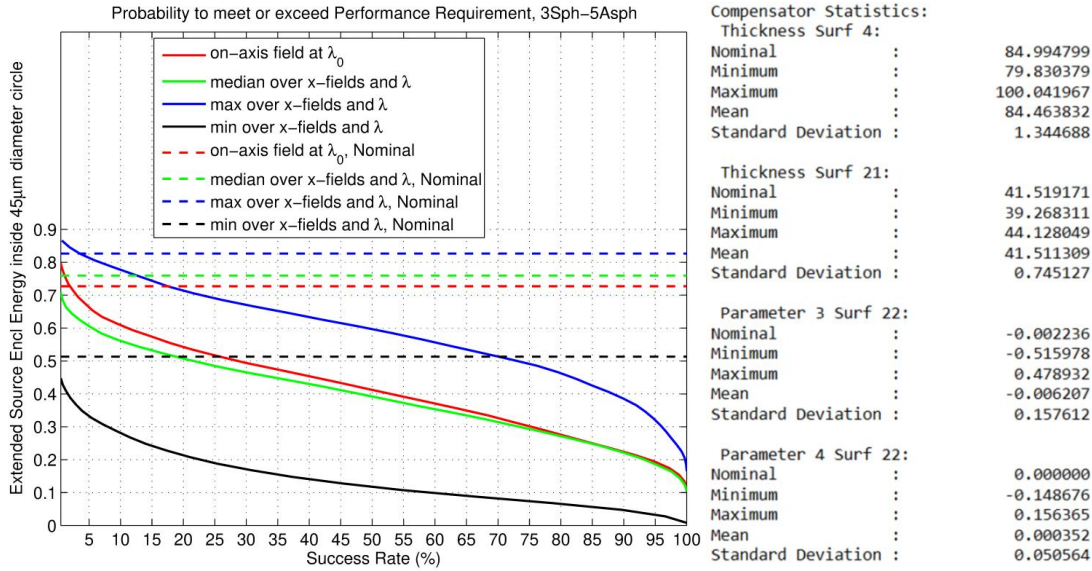


Figure 13: Monte Carlo tolerance results of the aspheric lens with grating. 1,000 Monte Carlo trials were performed with uniform opto-mechanical error statistics. Success rate is defined as the probability over simulation trials to meet or exceed a given performance level. Right: Compensator statistics for the 3Sph-5Asph design including the grating. The first group is pupil relief, the second is BFD and last two are image plane tilt about the x- and y-axis respectively.

4. REFLECTIVE CAMERA DESIGN

4.1 Design progression

Four- and five-mirror anastigmats (4MA, 5MA) have been discussed in the literature, for instance by Andrew Rackich [14] and Lacy Cook [15]. These imagers were invented to address fast and large field of view problems. Dave Shafer's high-performance 5MA design with external pupil served as our starting point [16]. It features a 300mm EPD, a 22deg FoV diameter, a focal ratio $f/2.0$ (600mm focal length averaged over fields), pupil relief (EP-M2 distance) is 600mm and image surface is flat. The surface sag of each mirror is described by an asymmetric general asphere [17]:

$$\begin{aligned}
 z(x, y) &\equiv \text{sag}(x, y) = \sum_{i=0}^{65} z_i(x, y), \\
 z_i(x, y) &= A_i \frac{x^{j(i)} y^{k(i)}}{R_n^o}, \\
 o(i) &= \text{floor}\left(\frac{\sqrt{1+8i}-1}{2}\right), \quad k(i) = i - \frac{o(o+1)}{2}, \quad j(i) = o - k, \quad i(k, o) = k + \frac{o(o+1)}{2}
 \end{aligned} \tag{1.21}$$

where i denotes the aspheric term number, z_i denotes the sag of aspheric term number i , o denotes the order of aspheric term i , j is the algebraic power of the local x coordinate on the surface, k is the algebraic power of the local y coordinate on the surface, and R_n is the normalization radius. x, y, z, A_i and R_n all have millimetre units. The mirror system is symmetric about the YZ plane, therefore the aspheric coefficients A_i are non-zero only for even powers of x (odd powers of x must be zero), which leads to a total 34 non-zero aspheric coefficients per mirror (order 10): order $o \geq 2$ has $N(o) = 1 + \text{floor}(o/2)$ non-zero terms, e.g. order 2 has 2 non-zero terms ($A_3 x^2 y^0 / R_n^2$), ($A_5 x^0 y^2 / R_n^2$), order 3

has 2 non-zero terms $(A_7 x^2 y^1 / R_n^3), (A_9 x^0 y^3 / R_n^3)$ etc. Even orders have only even powers of x and even powers of y , whereas odd orders have only even powers of x and odd powers of y . As a result, the OPD in the XP has zero projection onto Zernike modes with odd algebraic power in the cosine of the polar angle, i.e. Zernike modes proportional to $\cos(\phi), \cos^3(\phi), \cos^5(\phi), \cos^7(\phi), \dots$, i.e. modes proportional to odd algebraic powers of the x coordinates in the XP. Although manufacturing and optical testing of large freeform mirrors remain challenging, promising progress in those areas has recently been made [18],[19],[20],[21],[22].

- Step1. The 5MA was scaled to the desired 392mm focal length and 291mm EPD. Focal length was determined using the Power Field method (ring of real rays traced around the chief ray of each field point). The 5MA was first analyzed without the grating at the pupil plane and with FoV discretized into a 7×7 array of field points with $\theta_y = \{0^\circ, \pm 2.1^\circ, \pm 4.2^\circ, \pm 6.3^\circ\}$ and $\theta_x = \{0^\circ, 1^\circ, 2^\circ, 3^\circ, 4^\circ, 5^\circ, 6.6^\circ\}$ to cover half of FoV_x given in (1.16) and FoV_y given in (1.5). After optimization (62x62 rectangular array pupil discretization, RMS WFE optimization criterion, local DLS), the desired first-order properties were met but interferences between M1/M2, M3/M5, M2/M4, M1/M3, and M4/IMA were observed. To overcome the clearance issue, a set of weighted constraints was imposed on ray global Y-heights in the Merit Function:
 - Lowest point on M3 above highest point on M5,
 - Lowest point on M1 above highest point on M2,
 - Lowest point on M2 above highest point on M4,
 - Lowest point on M1 above highest point on M3,
 - Lowest point on M4 above highest point on IMA.
- Step2. After optimization of mirror spacings, X-tilts and aspheric coefficients, the number of non-zero aspheric coefficients per mirror was reduced to only 23 (orders 2 to 8) without performance loss.
- Step3. The grating was introduced at the pupil, 11 X-fields and 11 wavelengths were simulated, the MF was updated and the system was re-optimized.

4.2 Performance results

4.2.1 Nominal performance

In this Section, performance of the 5-mirror anastigmat (5MA) with the grating and fibers in the pseudo-slit is discussed. The optical layout is shown in Figure 14, the optical prescription in Figure 15 and performance results in Figure 16 and Figure 17. The merit function was built with uniform x-fields and wavelengths weights and optimization was performed using local DLS. All sample points have between 92% and 98% extended source enclosed energy within a 45microns diameter circle. Focus sensitivity and a field distortion map are displayed in Figure 18. The map was obtained by removing the diffraction grating. Maximum distortion is only -1.85%. Note that field distortion is not symmetric with respect to Y. Note also that the excellent imaging performance comes at the expense of poor intermediate pupil (located between M4 and M5) quality, but this is not of concern in spectrograph applications. No attempt has been done to optimize both image and pupil quality. In other applications (e.g. microlithography), variation in relative illumination across the image may have to be kept very low, therefore pupil size variations across the field may not be allowed and tight pupil size and pupil shape control may be required.

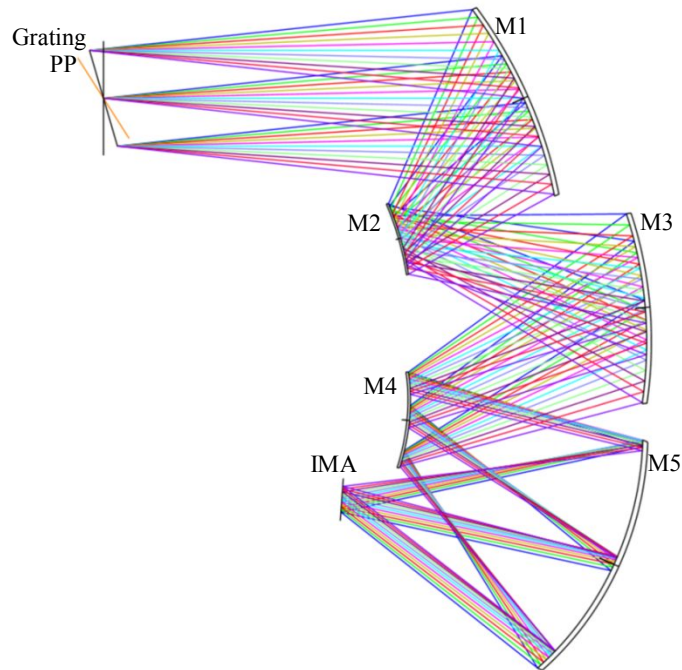


Figure 14: Optical layout and on-axis field Y-fan for the 5MA design including the grating. Short/long wavelength rays leave the pupil with positive/negative slope. The global coordinate reference surface is the vertex plane of the first mirror. Rays are colored by wavelength.

	Surf.Type	Comment	Radius	Thickness	Material	Semi-Diameter	Decenter X	Decenter Y	Tilt About X	Tilt About Y	Tilt About Z
0	OBJECT	Standard	Infinity	Infinity		Infinity					
1	STOP	Standard	Infinity	0.000000		145.500000 U					
2	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	32.560000	0.000000	0.000000
3	Standard		Infinity	0.000000		173.733767					
4	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	-32.560000	0.000000	0.000000
5	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	16.280000	0.000000	0.000000
6	Diffraction Grating	grating	Infinity	0.000000		152.466859	1.475000	-1.000000			
7	Coordinate Break	pupil relief	1622.506756 V	-		0.000000	0.000000	0.000000	16.270252	0.000000	0.000000
8	Standard		Infinity	0.000000		405.068419					
9	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	-21.937250 V	0.000000	0.000000
10	Extended Polynomial	M1	Infinity	0.000000	MIRROR	412.151262					
11	Coordinate Break		-670.173718 V	-		0.000000	0.000000	0.000000	-21.937250 P	0.000000	0.000000
12	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	29.872204 V	0.000000	0.000000
13	Extended Polynomial	M2	Infinity	0.000000	MIRROR	165.181792					
14	Coordinate Break		861.669272 V	-		0.000000	0.000000	0.000000	29.872204 P	0.000000	0.000000
15	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	-21.549102 V	0.000000	0.000000
16	Extended Polynomial	M3	Infinity	0.000000	MIRROR	368.263766					
17	Coordinate Break		-890.297769 V	-		0.000000	0.000000	0.000000	-21.549102 P	0.000000	0.000000
18	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	26.648513 V	0.000000	0.000000
19	Extended Polynomial	M4	Infinity	0.000000	MIRROR	173.437391					
20	Coordinate Break		836.061098 V	-		0.000000	0.000000	0.000000	26.648513 P	0.000000	0.000000
21	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	-9.757689 V	0.000000	0.000000
22	Extended Polynomial	M5	Infinity	0.000000	MIRROR	414.804641					
23	Coordinate Break		-777.913708 V	-		0.000000	0.000000	0.000000	-9.757689 P	0.000000	0.000000
24	Standard		Infinity	-94.534669 V		0.000000 U					
25	Coordinate Break		0.000000	-		0.000000	0.000000	0.000000	-4.892571 V	0.000000	0.000000
26	IMAGE	Standard	Infinity	-		62.626054					

Figure 15: Optical prescription for the 5MA design including the grating.

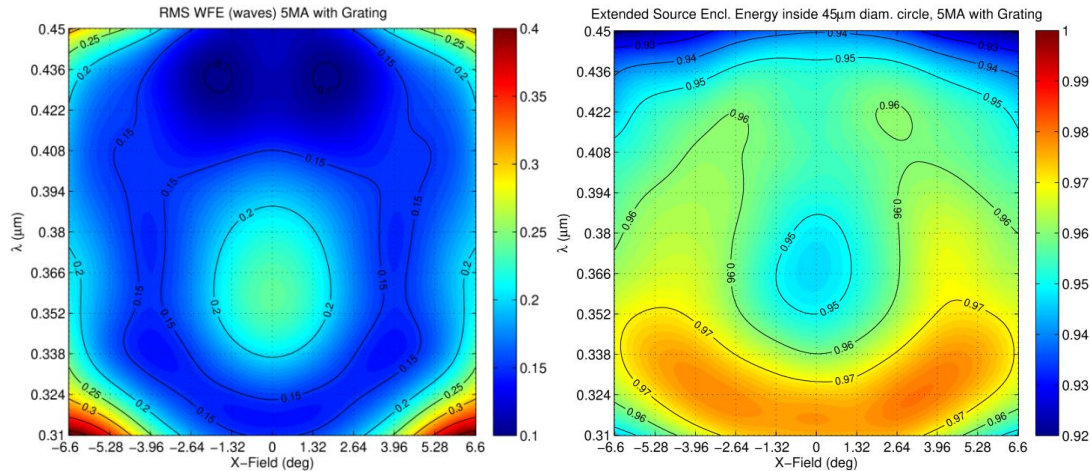


Figure 16: RMS WFE and extended source EE within 45μm diameter versus field and wavelength for the 5MA with grating.

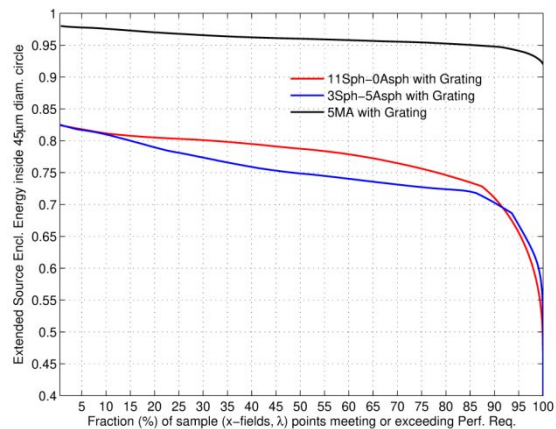


Figure 17: EE inside a 45micron diameter circle at the detector versus fraction of field and wavelength points meeting or exceeding a given performance level for the 11-element spherical lens with grating, the 8-element aspheric lens with grating, and the 5MA with grating.

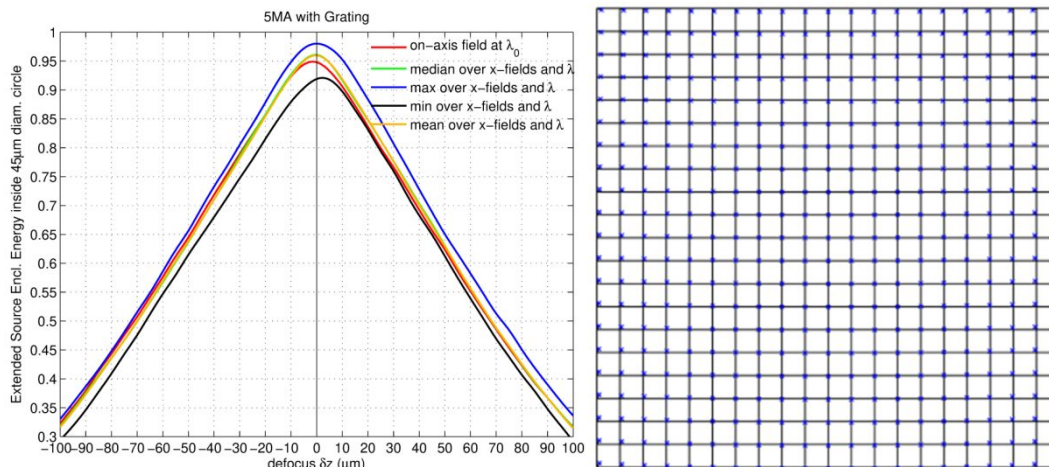


Figure 18: Left: Extended source EE within 45μm diameter versus defocus from nominal image plane position for the 5MA with grating. Right: Field distortion map for the 13.2deg (spatial direction) x 12.6deg (dispersion direction) FoV (1x scale factor), 92.6mm x 83.5mm. Maximum distortion is only -1.85%.

4.2.2 Tolerance analysis

The tolerances listed in Table 2 were imposed on the freeform 5MA (pending mechanical review).

Item	Value	Comment
Thickness (air)	$\pm 100\mu\text{m}$	
X and Y element decenter	$\pm 50\mu\text{m}$	twice Optimax high-precision thickness tolerance as an estimate for linear distance tolerance, pending mechanical review
Surface irregularity	$\pm 0.02\%$ of the nominal coefficient value for M1/M3/M4, $\pm 0.1\%$ of the nominal value for M2 and $\pm 0.003\%$ of the nominal value for M5.	Parabolic terms only: $(A_3x^2y^0/R_n^2), (A_5x^0y^2/R_n^2)$ Tolerances were obtained from inverse sensitivity analysis (nominal MF value was 2.08 and was allowed to increase up to 2.68). As shown in Table 3 these tolerances also correspond to the change in radius of curvature.
Element X and Y tilt	$\pm 0.0083\text{deg}$ ($\pm 0.5\text{arcmin}$)	Optimax wedge prism high precision

Table 2: Opto-mechanical tolerances adopted for the freeform 5MA tolerance analysis.

Four active compensation strategies were studied in 600 Monte Carlo simulation trials with uniform opto-mechanical error statistics:

- Active BFD adjustment (constrained between 50mm and 200mm),
- Active Pupil Relief adjustment (constrained between 1422mm and 1822mm),
- Active detector plane X- and Y-tilt adjustment (constrained between -15deg and +10deg).

Radii of curvature R_x and R_y along the x- and y-directions depend solely on the quadratic sag coefficients A_3 and A_5 respectively. The x-cross section of the parabolic sag component is given by $z_3 = A_3 \frac{x^2}{R_n^2} = \frac{c_x x^2}{2}$ where the last equality is obtained from the sag expression of a parabola ($K = -1$) and $c_x = 1/R_x$ is x-curvature and R_x the x-radius of curvature. We thus have $R_x = \frac{R_n^2}{2A_3} = -2f_x$ where f_x denotes the focal length for the x-direction. Denoting by $z_3' = A_3' \frac{x^2}{R_n^2} = \frac{c_x' x^2}{2}$ the parabolic sag along the x-direction for the perturbed coefficient $A_3' = A_3 + \text{tol}_3$, we have $R_x' = \frac{R_n^2}{2A_3'}$ and:

$$\frac{c_x}{c_x'} = \frac{R_x'}{R_x} = \frac{f_x'}{f_x} = \frac{A_3}{A_3'} = \frac{1}{1 + \frac{\text{tol}_3}{A_3}} \quad (1.22)$$

$$z_3'(x_{\max}) - z_3(x_{\max}) = (A_3' - A_3) \frac{x_{\max}^2}{R_n^2} = \text{tol}_3 \frac{x_{\max}^2}{R_n^2}$$

Similar equations apply to the parabolic term along the y-direction $z_5(y) = A_5 \frac{y^2}{R_n^2} = \frac{c_y y^2}{2}$. Table 3 presents the calculations performed to estimate the change in radius of curvature and the change in parabolic sag when the above tolerances are applied. It is worth noting that the change in radius of curvature (or equivalently focal length) is on the order of only 0.02% at the exception of M2 which has a relaxed radius tolerance of 0.1% and M5 with a tightened radius

tolerance of 0.03%. Figure 19 shows performance versus success rate (confidence level) for 600 Monte Carlo trials when the above opto-mechanical errors are applied with uniform statistics.

	M1	M2	M3	M4	M5	from lens data and tol data
normalization radius (mm)			0.643279			R_n
Ray X Max (mm)	336.7591	114.9712	299.9902	146.5281	350.5993	x (from footprint)
A3 (mm)	-1.480454E-04	-2.720384E-04	-1.561555E-04	-2.729770E-04	-2.024802E-04	(x/R_n)^2 coefficient
Nominal X Radius of Curvature (mm)	-1397.571	-760.569	-1324.987	-757.954	-1021.848	R=(R_n)^2/(2*A)
Nominal X Parabolic Sag (mm)	-40.5728	-8.6898	-33.9604	-14.1635	-60.1459	z= A*(x/R_n)^2
min tol3 (mm)	-3.538548E-08	-2.700000E-07	-4.956410E-08	-6.196211E-08	-6.910522E-09	tol
min tol3 / A3	2.390178E-04	9.925069E-04	3.174022E-04	2.269866E-04	3.412937E-05	tol/A
A3' (mm)	-1.480808E-04	-2.723084E-04	-1.562051E-04	-2.730390E-04	-2.024871E-04	A' = A + tol
Perturbed X Radius of Curvature (mm)	-1397.237	-759.815	-1324.566	-757.782	-1021.813	R'=(R_n)^2/(2*A')
Perturbed X Parabolic Sag (mm)	-40.5825	-8.6984	-33.9712	-14.1667	-60.1479	z'= A'*(x/R_n)^2
Change in X Radius of Curvature (%)	0.02	0.10	0.03	0.02	0.003	(R-R')/R*100 =(tol/A)/[1+(tol/A)]*100
Change in X Parabolic Sag (um)	9.698	8.625	10.779	3.215	2.053	(z-z')*1000=-tol*(x/R_n)^2*1000
Change in X Parabolic OPD (um)	19.395	17.249	21.558	6.430	4.105	2*(z-z')*1000
Change in X Parabolic OPD (waves @ 0.5um) (Nb. of fringes)	39	34	43	13	8	2*(z-z')*1000/vvl
Ray Y Max (mm)	344.1008	111.2554	274.4203	138.3533	357.0724	y (from footprint)
A5 (mm)	-1.264072E-04	-1.871564E-04	-1.344174E-04	-2.337881E-04	-1.988710E-04	(y/R_n)^2 coefficient
Nominal Y Radius of Curvature (mm)	-1636.805	-1105.514	-1539.265	-885.006	-1040.393	R=(R_n)^2/(2*A)
Nominal Y Parabolic Sag (mm)	-36.1697	-5.5982	-24.4618	-10.8144	-61.2753	z= A*(y/R_n)^2
min tol5 (mm)	-3.403932E-08	-1.800000E-07	-4.629989E-08	-5.536229E-08	-6.716893E-09	tol
min tol5 / A5	2.692831E-04	9.617625E-04	3.444486E-04	2.368054E-04	3.377513E-05	tol/A
A5' (mm)	-1.264412E-04	-1.873364E-04	-1.344637E-04	-2.338435E-04	-1.988777E-04	A' = A + tol
Perturbed Y Radius of Curvature (mm)	-1636.364	-1104.451	-1538.735	-884.797	-1040.358	R'=(R_n)^2/(2*A')
Perturbed Y Parabolic Sag (mm)	-36.1794	-5.6036	-24.4703	-10.8170	-61.2773	z'= A'*(y/R_n)^2
Change in Y Radius of Curvature (%)	0.03	0.10	0.03	0.02	0.003	(R-R')/R*100 =(tol/A)/[1+(tol/A)]*100
Change in Y Parabolic Sag (um)	9.740	5.384	8.426	2.561	2.070	(z-z')*1000=-tol*(y/R_n)^2*1000
Change in Y Parabolic OPD (um)	19.480	10.768	16.852	5.122	4.139	2*(z-z')*1000
Change in Y Parabolic OPD (waves @ 0.5um) (Nb. of fringes)	39	22	34	10	8	2*(z-z')*1000/vvl

Table 3: Change in radius of curvature and defocus OPD for each mirror of the 5MA with grating when tolerances listed in Table 2 are applied to the nominal parabolic X- and Y-sag coefficients.

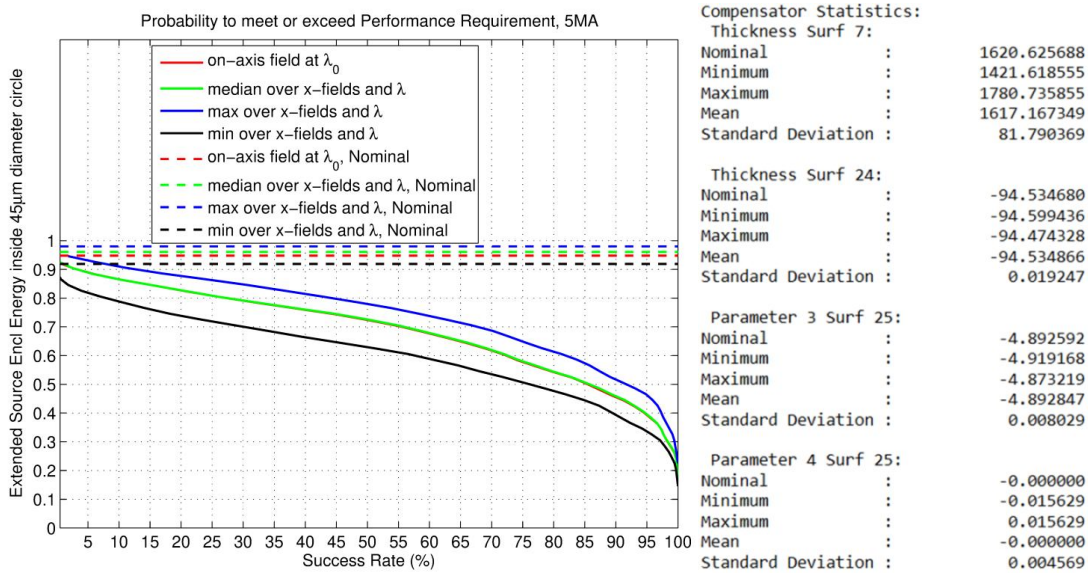


Figure 19: Monte Carlo tolerance results of the 5MA with grating. 600 Monte Carlo trials were performed with uniform opto-mechanical error statistics. Success rate is defined as the probability over simulation trials to meet or exceed a given performance level. Right: compensator statistics for the 5MA design including the grating. The first group is pupil relief, the second is BFD and last two are image plane tilt about the x- and y-axis respectively.

5. CATADIOPTIC CAMERA DESIGN

5.1 Design progression

Given the complexity of the refractive and reflective designs discussed, we deemed important to seek simpler solutions [23]. In this regard, an analysis of Bernard Delabre’s compact, fast, 3-element, catadioptric camera [24] has been performed. The camera was recently developed for the MOONS spectrograph of the VLT. First-order MOONS

parameters are close to the latest fiber WFOS parameters. The camera design consists of an aspheric concave mirror and an aspheric fused silica meniscus corrector lens glued to an aspheric fused silica convex-plano field flattener lens. Only the front surface of the corrector and field flattener lens is aspheric. Winlight [25] can manufacture such cameras using Luphos GmbH metrology equipment [26], which allows manufacturing of highly aspheric lenses and mirrors. The camera is extremely fast with a focal ratio of $f/0.95$, it has an external pupil of diameter equal to $D_{EP} = 280\text{mm}$ (focal length equal to $f_{cam} = 266\text{mm}$), and can accommodate a 4K detector with $15\mu\text{m}$ pixels (image width equal to

$l_y = l_x = 61\text{mm}$), i.e. $\text{FoV} = \text{FoV}_y = \text{FoV}_x = 2 \cdot \text{atan}\left(\frac{l_y}{2f_{cam}}\right) \cdot \frac{180}{\pi} \text{deg} = 13.1\text{deg}$. The main drawback of the camera is the vignetting due to the detector central obscuration. A good approximation for the vignetting amount is given by the ratio of the circular image area at the detector to the circular entrance pupil area. This ratio depends only on focal ratio and field of view and is given by:

$$v = \left(\frac{2f_{cam} \tan(\text{FoV}/2)}{D_{EP}} \right)^2 = 4f_{\#}^2 \tan^2(\text{FoV}/2) \quad (1.23)$$

For the MOONS camera's focal ratio and field of view, (1.23) yields 20% vignetting.

- The design was scaled to the desired 392mm focal length and 291mm EPD. The grating was introduced at the pupil, the MF was setup with 11 X-fields and 11 wavelengths, and the system was re-optimized. For the focal ratio given in (1.15) and field of view given in (1.18), (1.23) yields also 20% vignetting. Speeding up the camera to $f/1.17$ while keeping the same FoV would reduce vignetting to 15%.

5.2 Performance results

5.2.1 Nominal performance

In this Section, performance of the 3-element catadioptric camera with the grating and fibers in the pseudo-slit is discussed. The optical layout is shown in Figure 20, the optical prescription in Figure 21 and performance results in Figure 22 and Figure 23. The mirror (M1) has a diameter of 480mm.

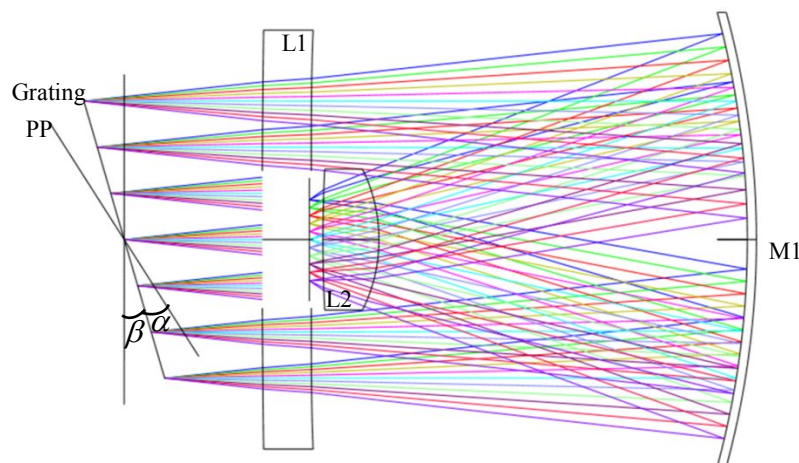


Figure 20: Optical layout and on-axis field Y-fan for the 3-element catadioptric design including the grating. Short/long wavelength rays leave the pupil with positive/negative slope. The global coordinate reference surface is the vertex plane of the first lens. Rays are colored by wavelength

	Surf.Type	Comment	Radius	Thickness	Material	Clear Semi-Dia	Mech Semi-Dia	Conic	2nd Order Ter	4th Order Term	6th Order Term	8th Order Term
0	OBJECT	Standard	Infinity	Infinity		Infinity	Infinity	0.000000				
1	STOP	Standard	Infinity	0.000000		145.500000	145.500000	0.000000				
2	Coordinate Break			0.000000	-	0.000000	-		0.000000	0.000000	32.560000	0.000000
3	Standard		Infinity	0.000000		173.352523	173.352523	0.000000				
4	Standard		Infinity	0.000000		173.352523	173.352523	0.000000				
5	Coordinate Break			0.000000	-	0.000000	-		0.000000	0.000000	-32.560000	0.000000
6	Coordinate Break			0.000000	-	0.000000	-		0.000000	0.000000	16.280000	0.000000
7	Diffraction Grating	grating	Infinity	0.000000		152.168433	-	0.000000	1.475000	-1.000000		
8	Coordinate Break	pupil relief		161.066952 V	-	0.000000	-		0.000000	0.000000	16.270252	0.000000
9	(aper)	Standard	1.627489E+04	51.614528	CAF2	174.772449	220.000000	0.000000				
10	(aper)	Even Asphere	-3.789523E+04	457.993123		179.505379	220.000000	0.000000	0.000000	9.582073E-10	2.298253E-15	0.000000
11	(aper)	Even Asphere	-919.432598	-386.977906	MIRROR	240.726668	240.726668	0.000000	0.000000	-5.918060E-11	-2.663039E-17	0.000000
12	(aper)	Even Asphere	-169.679882	-58.855147	CAF2	74.000000 U	74.000000	0.000000	0.000000	-1.132239E-08	1.051974E-13	0.000000
13	(aper)	Standard	1430.802603	0.000000		74.000000 P	74.000000	0.000000				
14	Standard		Infinity	-14.299155 V		74.800744	74.800744	0.000000				
15	Coordinate Break			0.000000	-	0.000000	-		0.000000	0.000000	9.559910E-04 V	4.018475E-03 V
16	IMAGE	Standard	Infinity	-		64.633432	64.633432	0.000000				

Figure 21: Optical prescription for the 3-element catadioptric design including the grating.

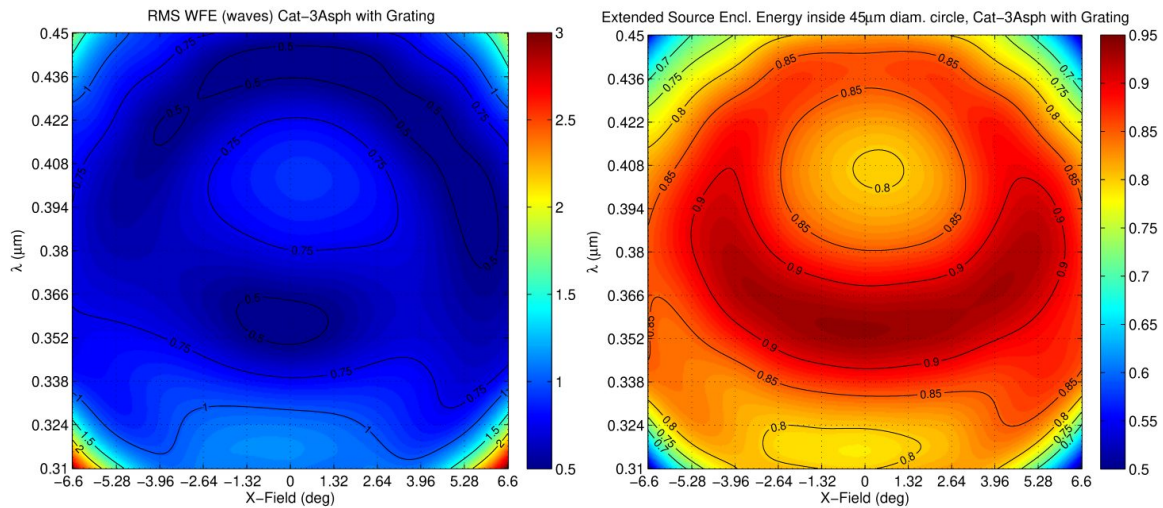


Figure 22: RMS WFE and extended source EE within 45µm diameter versus field and wavelength for the 3-element catadioptric design with grating.

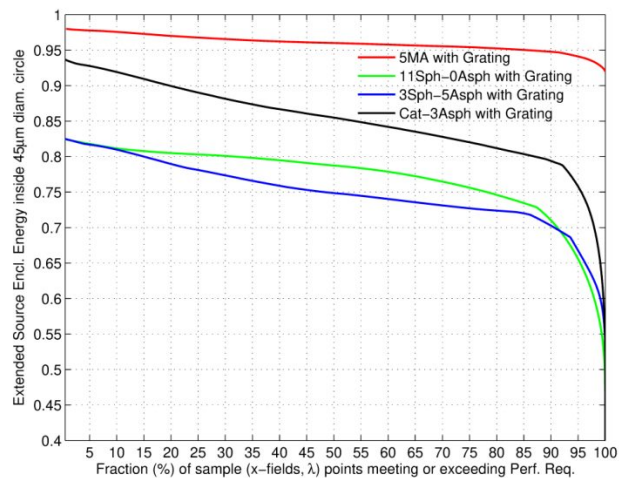


Figure 23: EE inside a 45micron diameter circle at the detector versus fraction of field and wavelength sample points meeting or exceeding a given performance level for the 11-element spherical lens with grating, the 8-element aspheric lens with grating, the 5MA with grating, and the 3-element catadioptric design.

5.2.2 Tolerance analysis

The tolerances listed in Table 1 were imposed on the catadioptric design. Four active compensation strategies were studied in 1,000 Monte Carlo simulation trials with uniform opto-mechanical error statistics:

- Active BFD adjustment,
- Active Pupil Relief adjustment,
- Active detector plane X- and Y-tilt adjustment.

Figure 24 shows Monte Carlo tolerance results, which indicate that the 3-element catadioptric design is robust against the opto-mechanical errors listed in Table 1. This design is therefore superior to the refractive and reflective designs investigated when performance is balanced against robustness to opto-mechanical errors.

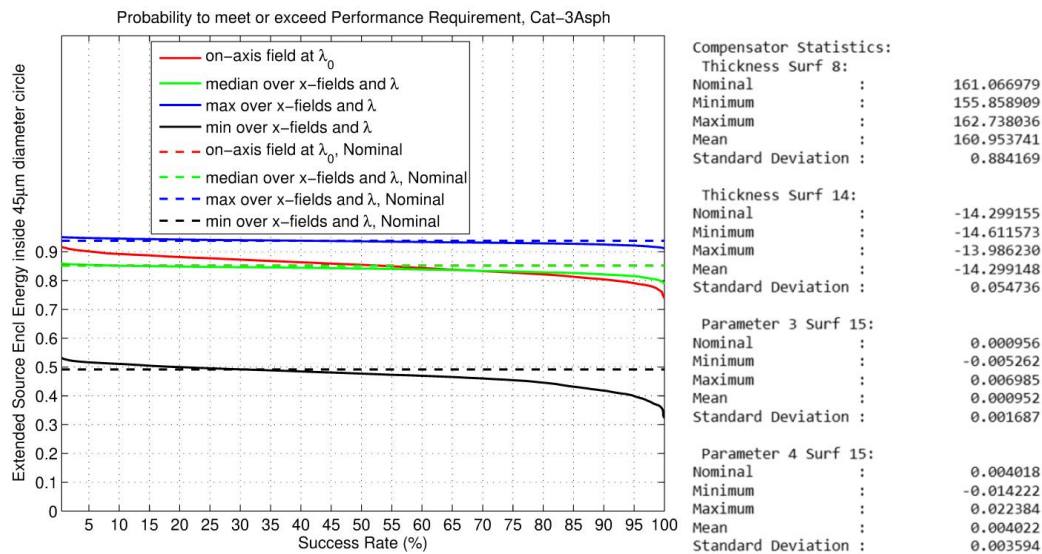


Figure 24: Monte Carlo tolerance results for the 3-element catadioptric camera with grating. 1,000 Monte Carlo trials were performed with uniform opto-mechanical error statistics. Success rate is defined as the probability over simulation trials to meet or exceed a given performance level. Right: compensator statistics for the 3-element catadioptric camera including the grating. The first group is pupil relief, the second is BFD and last two are image plane tilt about the x- and y-axis respectively.

6. CONCLUSIONS

In this paper, 2 refractive designs, 1 reflective freeform design, and 1 catadioptric design were investigated for the UV camera of the TMT fiber WFOS instrument concept based on first-order instrument parameters provided in August 2017. All 4 camera designs could easily be re-optimized for the latest fiber WFOS parameters if needed.

The camera full FoV along the spatial (X) direction is 13.2° and 12.6° along the dispersion (Y) direction, the EPD is 291mm and the stop is external, the focal length is 392mm (the paraxial focal ratio is $f/1.35$ at the primary wavelength $\lambda_0 = 0.38\mu\text{m}$). The blue channel covers wavelengths ranging from $\lambda_1 = 0.31\mu\text{m}$ to $\lambda_2 = 0.45\mu\text{m}$. The spectrograph magnification is $m = -f_{\text{cam}} / f_{\text{col}} = -0.45$. Fibers are 100microns in diameter, and the grating has a period equal to $\nu = 1.475$ lines/micron, which leads to a 16.275° grating tilt in Littrow configuration.

The top-level end-to-end performance requirement for the instrument is 90% extended source encircled energy (EE) inside a 45micron diameter circle on the detector for a 100micron diameter object (fiber core diameter), which for the chosen collimator focal length, corresponds to a fiber angular diameter of 23.65arcsec .

- Custom macros were written to compute in post-processing extended source enclosed energy and RMS WFE maps as a function of x-fields (fibers in the pseudo-slit) and wavelengths. Data analysis and visualization was performed using Matlab.
- Nominal performance results are displayed in Figure 23. Both refractive designs provide 70% encircled energy inside a fiber over 90% of x-fields and wavelengths, whereas the 3-element catadioptric camera is able to achieve 80% and the freeform 5MA 95% encircled energy over the same percentage of x-fields and wavelengths.
- Because of its speed, the camera is very sensitive to defocus: $\pm 20\mu\text{m}$ axial shift of the detector about its nominal position produces a 10% encircled energy loss. Similarly, $\pm 0.1\text{deg}$ detector tilt about its nominal position produces also a 10% encircled energy loss.
- A tolerance analysis was carried out for each design. Monte Carlo simulation results with high-precision opto-mechanical tolerances applied are displayed for the spherical lens in Figure 8, for the aspheric lens in Figure 13, for the 5MA in Figure 19, and for the 3-element catadioptric camera in Figure 24. For the tolerances analyzed (pending mechanical review), for a 95% success rate (confidence level), the spherical lens exhibits a median extended source encircled energy over x-fields and wavelengths of only 30%, the aspheric lens of only 20%, the 5MA of only 40%, and the 3-element catadioptric lens of 83%. The 3-element catadioptric design, despite its 20-25% vignetting, is therefore superior to the refractive and reflective designs investigated when performance is balanced against robustness to opto-mechanical errors. Refinement of tolerances is needed after iteration with mechanical engineering and review of manufacturing capabilities. Although providing exquisite nominal performance, the 5MA design suffers from higher sensitivity to sag and tilt errors than the refractive and catadioptric designs. This can be understood in light of the fact that for a mirror, power is proportional to twice the sag (double pass effect), whereas for a lens the proportionality factor is the index minus one, which is about 4x smaller than for a mirror.

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